



## Thermal and diffusion Cattaneo-Christov heat flux models on Walter's-B Buongiorno nanofluid over an electromagnetic surface with second order velocity slip.

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### Abstract

The intension of the current study is to explore optimization in heat transfer using Cattaneo-Christovs thermal and the solutal diffusions along with heat source/sink which are non-uniform on a stagnation points flow of nanoWalter's B fluid over an electromagnetic sheet subjected to the multiple slip mechanisms. This study also scrutinizes the role of electromagnetic fields. The flow equations are modified via incorporating suitable transformations into a self-similarity equalities. Further numerically solved by employing Runge-Kutta method of shooting technique. The acquired results shows good agreement with the previous published works. The noteworthy findings are- Walter's B nanofluid which flow parallel to the electromagnetic sheet is assisted by the Lorentz force. Electromagnetic sheet can be used for better cooling since improvement in Hartmann declines thermal boundary layer. Augmentation in thermal, velocity, and the solutal slip parameter shrink the hydrodynamic, solutal and thermal boundary layer.

**Keywords:** Cattaneo-Christov, Walter's B fluid, Buongiorno nanofluid, non-uniform Heat Sink/Source, 2nd order velocity slips, concentration slip, thermal slip.

### 1. Introduction.

The present technological development in the electronics industry along with the advanced energy density devices are accompanied with the thermal management encounters. It is estimated that the heat fluxes in most of these system are anticipated to go beyond  $100 \text{ W/cm}^2$ . Hence, cooling technologies containing the MCHS are continually upgraded in order to handle the associated thermal challenges. Some of these methods include usage of functionally graded materials, geometric optimization of the heat exchangers and incorporating the nanofluid as the working fluid. Nanofluid is obtained via integrating ultrafine nanoparticles comprising of mainly oxides, metals and other compounds in the heat transport fluids. Recently, researchers [1-5] explored nanofluid focusing primarily on the viscosity, stability electrical and thermal performances. Buongiorno [6] suggested a nanofluid model incorporating the Brownian - thermophoresis motion properties. Recently, researchers [7-10] scrutinized the thermal conductivity behavior by incorporating Buongiorno model. In Industrial and the engineering procedures, to obtain the best quality product accurate knowledge of heat transfer procedure is very much essential. In the past most of the researchers and engineers applied Fourier's heat conduction law on order to study heat transport traits. In Recent times Liu et al. [11] and Qi and Guo [12] had a concern that Fourier's heat conduction law [13] produces parabolic energy equation thus any kind of initial disturbance would affect the whole system. Thus after the primary work of Cattaneo [14] followed by Christov [15] a new model for heat flux called Cattaneo-Christov is constituted to study heat transfer features. Currently, researchers



[16-20] explored the heat transfer nature by incorporating Cattaneo-Christov double -diffusion hypothesis over various surfaces.

No-slip condition is recurrently employed in flow of viscous fluid problems. However, in certain circumstances slip may arise at the boundary when the fluid is particulate for example suspensions, polymer, emulsions and foam solutions. Further, no-slip conditions is not valid for the flow which take place at micro and nanoscale hence, a certain degree of tangential slip should be allowed. In view of this phenomenon recently researchers [21-25] investigated flow and heat transfer by considering partial and second order slip.

Gailitis and Lielausis [26] invented a device to generate the exponentially decomposing wall-parallel Lorentz force. This device is the electromagnetic actuator containing electrodes and permanent magnet Thus the electromagnetic body force produced due to stretching manages the flow separations and eradicate the turbulence influence developing in the flow. Researchers [27-32] investigated flow over the Riga-plate.

Through the above stated literature survey the researchers here are interested in investigating the influence of Cattaneo Christov solutal and thermal diffusions along with the non-uniform heat source-sink on the stagnation point flows of nanoWalter’s B fluid over the electromagnetic sheet subjected to the slip mechanisms. The flow model are converted by incorporating self-similarity equations and then numerically handled through the Runge-Kutta shooting method.

**2. Mathematical formulation.**

The Present exploration deals with stagnation point flow of a Walter’s B fluid over an electromagnetic sheet. Effect of Buongiorno nanofluid, Cattaneo-Christov heat along with mass flux and non-uniform heat source-sink is taken into consideration. A Cartesian coordinate system originate from leading edges of the electromagnetic sheet. The geometry of the flow problem is portrayed in Figure 1.

The boundary layer equations referring Nayak et al. [28] Shafiq et al. [31] and Ahmad et al. [27] are:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial v}{\partial y} = \left( \left( \frac{\zeta_0}{\rho_f} \right) \frac{\partial^2 u}{\partial y^2} + u_\infty \frac{\partial u_\infty}{\partial x} - \frac{k_0}{\rho_f} \left( v \frac{\partial^3 u}{\partial y^3} + u \frac{\partial^3 u}{\partial x \partial y^2} - \frac{\partial u}{\partial y} \frac{\partial^2 u}{\partial x \partial y} + \frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial y^2} \right) \right) + \left( \frac{\pi j_0 M_0}{8 \rho_f} \right) e^{(-\pi/\lambda)y} \tag{2}$$



$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + \Delta_T \left[ \begin{array}{l} u^2 \frac{\partial^2 T}{\partial x^2} + u \frac{\partial u}{\partial x} \frac{\partial T}{\partial x} + \\ u \frac{\partial v}{\partial y} \frac{\partial T}{\partial y} + v^2 \frac{\partial^2 T}{\partial y^2} \\ + v \frac{\partial u}{\partial y} \frac{\partial T}{\partial x} + v \frac{\partial v}{\partial y} \frac{\partial T}{\partial y} \\ + 2uv \frac{\partial^2 T}{\partial x \partial y} \end{array} \right] = \frac{k_f}{(\rho c_p)_f} \frac{\partial^2 T}{\partial y^2} + \left[ \begin{array}{l} \tau D_B \frac{\partial C}{\partial y} \frac{\partial T}{\partial y} + \frac{D_T}{T_\infty} \left( \frac{\partial T}{\partial y} \right)^2 + \\ \left( \frac{ku_w(x)}{xv} \right) \left( A^* (T_w - T_\infty) \right. \\ \left. F'(\zeta) B^* (T - T_\infty) \right) \end{array} \right] \quad (3)$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} + \Delta_C \left[ \begin{array}{l} u^2 \frac{\partial^2 C}{\partial x^2} + u \frac{\partial u}{\partial x} \frac{\partial C}{\partial x} + u \frac{\partial v}{\partial y} \frac{\partial C}{\partial y} + v^2 \frac{\partial^2 C}{\partial y^2} \\ + v \frac{\partial u}{\partial y} \frac{\partial C}{\partial x} + v \frac{\partial v}{\partial y} \frac{\partial C}{\partial y} + 2uv \frac{\partial^2 C}{\partial x \partial y} \end{array} \right] = D_B \frac{\partial^2 C}{\partial y^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial y^2} \quad (4)$$

Boundary conditions are:

$$\text{At } y=0, \quad u = u_w(x) + A \left( \frac{\partial u}{\partial y} \right) + B \left( \frac{\partial^2 u}{\partial y^2} \right), \quad v = 0, \quad T = T_w + L \left( \frac{\partial T}{\partial y} \right), \quad C = C_w + M \left( \frac{\partial C}{\partial y} \right) \quad (5)$$

$$\text{As } y \rightarrow \infty, \quad u \rightarrow u_\infty(x) = cx, \quad T \rightarrow T_\infty, \quad C \rightarrow C_\infty \quad (6)$$

Here,  $\zeta_0$  is limiting viscosity at the small shear rate,  $k_0$  is elastic parameter,  $j_0$  is current density,  $g$  is gravitational acceleration,  $M_0$  is magnetization of permanent magnets,  $k_f$  is thermal

conductivity,  $l$  is width of electrodes and magnets,  $\tau = \left( \frac{(\rho C_p)_p}{(\rho C_p)_f} \right)$  heat capacity ratios,  $\Delta_T$  is

thermal relaxation time,  $\Delta_C$  is solutal relaxation time,  $D_B$  Brownian diffusions and  $D_T$  is thermophoretic diffusion coefficient,  $A, B, L, M$  are velocity slip constant, thermal slip constant and concentration slip constant,

In the equation (3)  $A^*$  and  $B^*$  are the coefficient of space and temperature heat source/sink and  $A^* > 0, B^* > 0$  relate to the internal heat generation.  $A^* < 0, B^* < 0$  Relate to internal heat absorptions.

Similar to Nayak et al. [28], the stream function and the subsequent similarity variable considered are:



$$\left. \begin{aligned} \psi(x, y) &= x\left(\sqrt{av_f}\right)F(\zeta), \quad \zeta = \left(\sqrt{\frac{a}{v_f}}\right)y \\ u &= axF'(\zeta), \quad v = -\left(\sqrt{av_f}\right)F(\zeta) \\ T &= T_\infty + (T_w - T_\infty)\theta(\zeta), \quad C = C_\infty + (C_w - C_\infty)\phi(\zeta) \end{aligned} \right\} \quad (7)$$

$\zeta$  is non-dimensional vertical distance and  $F(\zeta)$  denotes stream function.

Thus by using (7) governing equations of motion (1)-(6) is reduced to the similarity form as:

$$\Gamma_1 \frac{d^3 F}{d\zeta^3} + \Gamma_2 \left[ 2 \frac{dF}{d\zeta} \frac{d^3 F}{d\zeta^3} - \frac{dF}{d\zeta} \frac{d^4 F}{d\zeta^4} - \left( \frac{d^2 F}{d\zeta^2} \right)^2 \right] + F(\zeta) \frac{d^2 F}{d\zeta^2} - \left( \frac{dF}{d\zeta} \right)^2 + \varepsilon^2 + Ze^{-\delta\zeta} = 0 \quad (8)$$

$$\frac{d^2 \theta}{d\zeta^2} + \text{Pr} \left[ \begin{aligned} & (Nb) \frac{d\theta}{d\zeta} \frac{d\phi}{d\zeta} + (Nt) \left( \frac{d\theta}{d\zeta} \right)^2 + F(\zeta) \frac{d\theta}{d\zeta} - \\ & R_T \left( \left( \frac{d^2 \theta}{d\zeta^2} \right) (F(\zeta))^2 + F(\zeta) \frac{dF}{d\zeta} \frac{d\theta}{d\zeta} \right) \end{aligned} \right] + B^* \theta(\zeta) + A^* \frac{dF}{d\zeta} = 0 \quad (9)$$

$$\frac{d^2 \phi}{d\zeta^2} + \left( \frac{Nt}{Nb} \right) \frac{d^2 \theta}{d\zeta^2} + Sc \left[ F(\zeta) \frac{d\phi}{d\zeta} - R_C \left( \left( \frac{d^2 \phi}{d\zeta^2} \right) (F(\zeta))^2 + F(\zeta) \frac{dF}{d\zeta} \frac{d\phi}{d\zeta} \right) \right] = 0 \quad (10)$$

$$\left. \begin{aligned} \frac{dF(0)}{d\zeta} &= 1 + \Upsilon_1 \frac{d^2 F(0)}{d\zeta^2} + \Upsilon_2 \frac{d^3 F(0)}{d\zeta^3}, \quad F(0) = 0, \quad \theta(0) = 1 + \Upsilon_3 \frac{d\theta(0)}{d\zeta}, \quad \phi(0) = 1 + \Upsilon_4 \frac{d\phi(0)}{d\zeta} \\ \frac{dF}{d\zeta}(\infty) &= \varepsilon, \quad \theta(\infty) \rightarrow 0, \quad \phi(\infty) \rightarrow 0 \end{aligned} \right\} \quad (11)$$

Here,

$$\Gamma_1 = \frac{\zeta_0}{\mu_f}, \quad \Gamma_2 = \frac{ak_0}{\mu_f}, \quad \delta = \frac{\pi}{\Lambda \sqrt{\frac{a}{v_f}}}, \quad Z = \frac{\pi j_0 Mx}{8\rho_f u_w^2}, \quad R_C = a\Delta_C, \quad R_T = a\Delta_T, \quad \varepsilon = \frac{c^2}{a^2}, \quad \Upsilon_1 = A \sqrt{\frac{a}{v_f}},$$

$$Nb = \frac{(\rho c_p)_p D_B (C_w - C_\infty)}{v_f (\rho c_p)_f}, \quad Nt = \frac{(\rho c_p)_p D_T (T_w - T_\infty)}{v_f (\rho c_p)_f}, \quad \Upsilon_2 = B \sqrt{\frac{a}{v_f}}, \quad \Upsilon_3 = L \sqrt{\frac{a}{v_f}}, \quad \Upsilon_4 = M \sqrt{\frac{a}{v_f}}$$

$$\text{Pr} = \frac{v_f (\rho c_p)_f}{k_f}, \quad Sc = \frac{v_f}{D_B}$$

$\Gamma_1, \Gamma_2, Z, \varepsilon, \delta, R_C, R_T, \Upsilon_1, \Upsilon_2, \Upsilon_3, \Upsilon_4, Nb, Nt, \text{Pr}, Sc$  is viscosity ratio parameter, viscoelastic parameter, Hartmann number, velocity ratio parameter, parameter signifying width of magnets and electrodes, solutal relaxation parameter, thermal relaxation parameter, first order and second



order velocity slip, thermal slip and solutal slip parameter, Brownian motion parameter, thermophoresis parameter, Prandtl number, Schmidt number.

The frictional drag ( $C_{f_x}$ ) is (see Qayyum et al. [30] and Hakeem et al. [35]):

$$C_{f_x} = \frac{\tau_w}{\frac{1}{2} \rho_f u_w^2} \tag{12}$$

$$\tau_w = \left[ \nu \left( \frac{\partial u}{\partial y} \right) - k_0 \left( \left( u \frac{\partial^2 u}{\partial x \partial y} \right) - \left( 2 \frac{\partial u}{\partial x} \frac{\partial u}{\partial y} \right) \right) \right]_{y=0}$$

Nusselt number ( $Nu_x$ ) is given by

$$Nu_x = \frac{xq_w}{k(T_w - T_\infty)} \tag{13}$$

$$q_w = -k \left( \frac{\partial T}{\partial y} \right)_{y=0}$$

The local Sherwood number ( $Sh_x$ ) is given by

$$Sh_x = \frac{xj_w}{D_B(C_w - C_\infty)} \tag{14}$$

$$j_w = -D_B \left( \frac{\partial C}{\partial y} \right)_{y=0}$$

In dimensionless form, the  $C_{f_x}$ ,  $Nu_x$  and  $Sh_x$  are

$$\text{Re}_x^{\frac{1}{2}} C_f = 2 \left( 1 + \Gamma_2 \left( \frac{dF(0)}{d\zeta} \right) \right) \frac{d^2 F(0)}{d\zeta^2}, \quad Nu_x = -\frac{d\theta(0)}{d\zeta} \text{Re}_x^{\frac{1}{2}} \tag{15}$$

$$Sh = -\frac{d\phi(0)}{d\zeta} \text{Re}_x^{\frac{1}{2}}$$

Here,  $\text{Re}_x = \frac{xu_w}{\nu_f}$

### 3. Calculation

To solve numerically the nonlinear Eqs. (8) – (11) shooting method (Runge–Kutta) is implemented in the MATLAB package. Results are tabulated in Table 1-4. The achieved effects are in exceptional concurrence with the available results. (See, of Nayak et al. [28] Hakeem et al. [35], Awais et al. [34] and Nadeem et al. [33]). Physical nature of assorted variables on velocities  $F'(\zeta)$ , temperature  $\theta(\zeta)$  and concentration  $\phi(\zeta)$  are elaborated through the Figures 2-18 and



in Table 4. deviation in  $\left(\frac{1}{2} C_{fx} \text{Re}_x^{1/2}\right)$  friction coefficient ,  $\left(\frac{1}{2} Nu_x \text{Re}_x^{-1/2}\right)$  Nusselt number and  $\left(\frac{1}{2} Sh_x \text{Re}_x^{-1/2}\right)$  Sherwood number are addressed.

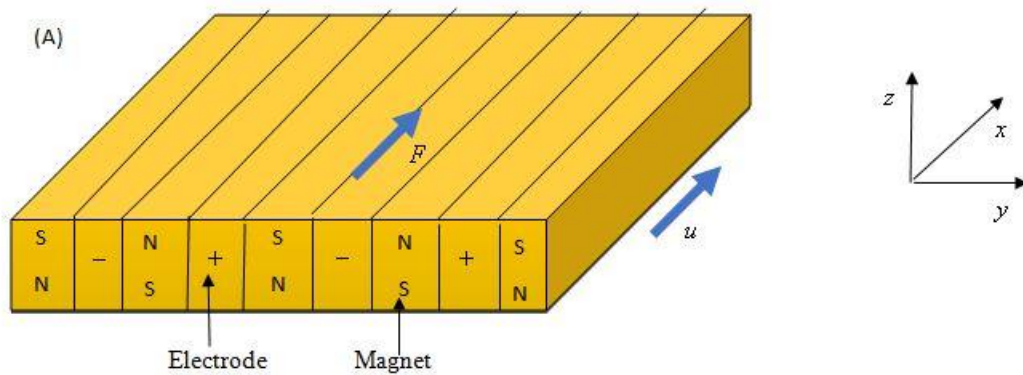
#### 4. Results and discussion

Figure 2. demonstrates the influence of modified Hartmann number ( $Z$ ) on the velocity profile  $F'(\zeta)$ . It shows that improving values of  $Z$  improves  $F'(\zeta)$  hence the associated thickness of the boundary layer improves. It infers that flow in positive  $x$ -direction on the electromagnetic sheet is encouraged by the surface parallel Lorentz forces. As expected, it is observed in Figure 3. that the augmentation in  $Z$  the surface parallel Lorentz forces which has assisted the flow field decreased the temperature  $\theta(\zeta)$ . Hence the electromagnetic sheet can be used for better cooling effect. Temperature profiles  $\theta(\zeta)$  are plotted for various values of thermal relaxation parameter ( $R_t$ ) in Fig. 4. Larger values of  $R_t$  decrease the  $\theta(\zeta)$  (temperature) and accompanying boundary layer thickness. In Figure 5. it is pragmatic that increment in solutal relaxation parameter ( $R_c$ ) improves the concentration of the nanofluid. Through Figure 6. it is observed that improvement in the ( $Nb$ ) Brownian motion parameter as anticipated enhances the temperature  $\theta(\zeta)$  of the nanofluid. This is because random motion of the fluid particles generates more heat within the frame thus one can notice thermal layer thickness as  $Nb$  improves. But for larger  $Nb$  the collision among the fluid particle increase which results in depreciation of the concentration field which is revealed in Figure 7. Figure 8. and Figure 9. Illustrates the influence of ( $Nt$ ) thermophoresis parameter on  $\theta(\zeta)$  temperature and  $\phi(\zeta)$  concentration field. Larger  $Nt$  give rise to higher thermal conductivity thus there is improvement in  $\theta(\zeta)$  profiles. Larger  $Nt$  initially near the boundary depreciates the concentration of the fluid but at  $\zeta \geq 1.5$  concentration  $\phi(\zeta)$  profiles improves. Through Figure 10. One can witness the temperature field on temperature dependent heat source-sink. As anticipated  $\theta(\zeta)$  temperature in the thermal boundary layer improves with increase in  $A^*$ . Similar behavior in concentration field is noticed through Fig. 11 with increase in  $A^*$ . In Figure 12. it is detected that the boundary layer thickness  $\theta(\zeta)$  declines initially near the boundary  $\zeta \leq 0.5$  further improves for increase in  $B^* \geq 0$ . This is because improvement in internal heat generation. Figure 13. Figure 14. and Figure 15 signifies the influence of rising values of the  $\delta$  (width of magnets and electrodes) it is perceived that enlargement in  $\delta$  improves the  $\theta(\zeta)$  temperature and associated boundary layer thickness and depreciates concentration and velocity of the nanofluid. Thus, for additional heating purpose thickness of magnets and electrodes could be increased. Figure 16. indicates the influence of increase in first order velocity slip  $\Upsilon_1$  parameter on  $F'(\zeta)$  velocity profiles. It is



notified that near the boundary for  $\zeta < 1$  velocity  $F'(\zeta)$  and associated boundary layer thickness decreases however whenever the magnitude of  $\Upsilon_1$  increased far away from the boundary  $\zeta \geq 1$  one can identify improvement in velocity  $F'(\zeta)$  and associated boundary layer thickness. In Figure 17 and 18 one can depict the influence of  $\Upsilon_3$  is thermal slip parameter,  $\Upsilon_4$  solutal slip parameter on temperature and concentration of the nanofluid. As the magnitude of slip  $\Upsilon_3$  and  $\Upsilon_4$  improves associated boundary layer falls and there is decline in temperature and concentration of the nanofluid.

Through the Table 4. One can observe Variation in skin friction  $\left(\frac{1}{2}C_{fx} Re_x^{1/2}\right)$ , Nusselt number  $\left(\frac{1}{2}Nu_x Re_x^{-1/2}\right)$  and Sherwood number  $\left(\frac{1}{2}Sh_x Re_x^{-1/2}\right)$  for sundry physical variables. It is evident that improvement in  $Z$  and  $\Upsilon_1$  improves the skin friction. Larger values of physical variables  $Z, R_T, R_C, A^*, B^*$  and  $\Upsilon_4$  improves heat transfer rate and  $Nb, Nt, \delta, \Upsilon_1, \Upsilon_3$  declines heat transfer performance. Mass transfer performance is improved with elevating values of physical variables  $Nb, Nt, A^*, B^*, \delta, \Upsilon_1, \Upsilon_3$  and  $Z, R_T, R_C, \Upsilon_4$  declines mass transfer rate.



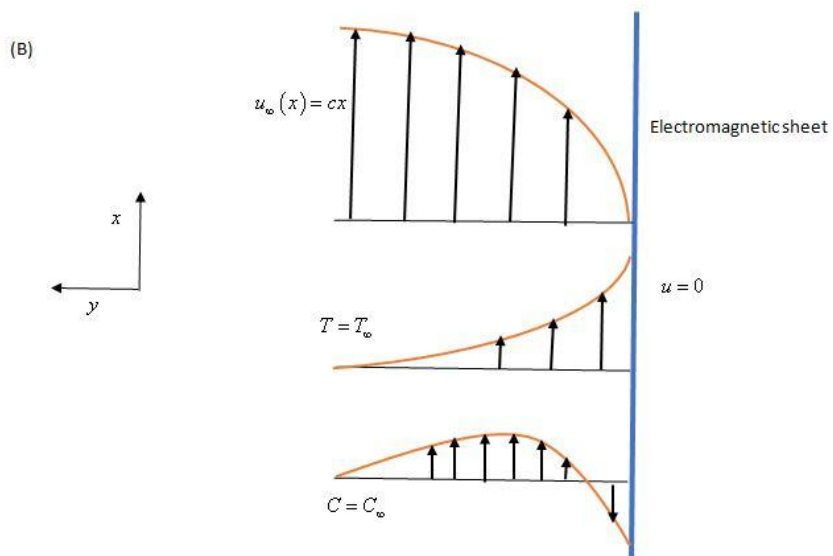


Figure 1. Physical configuration of the flow problem

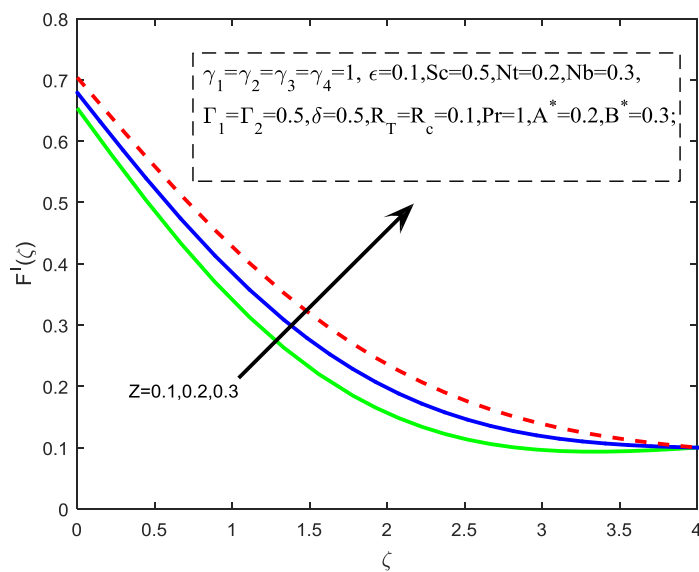


Figure 2. Influence of  $z$  on  $F'(\zeta)$  velocity profile



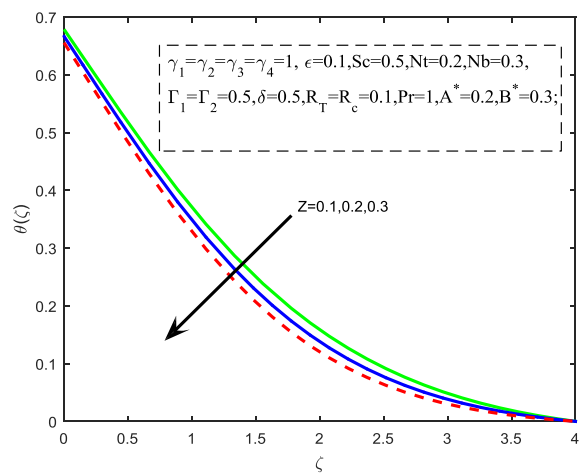


Figure 3. Influence of  $z$  on  $\theta(\zeta)$  temperature profile

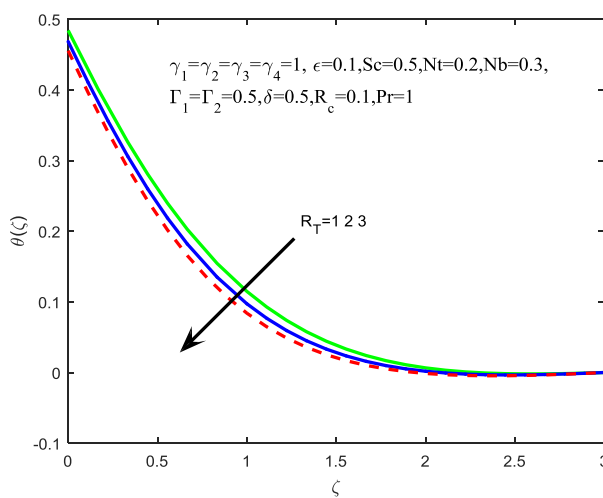


Figure 4. Influence of  $R_T$  on  $\theta(\zeta)$  temperature profile

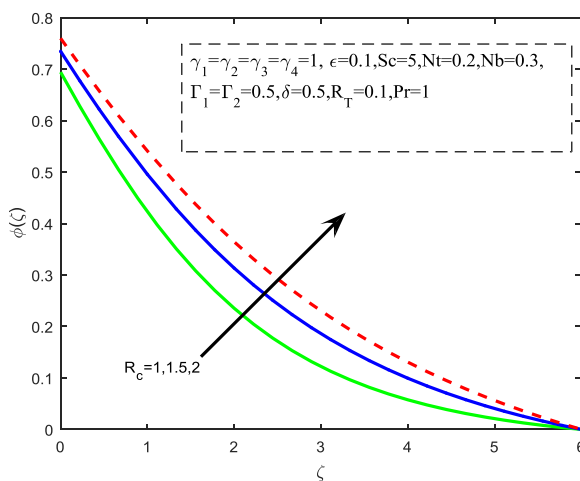


Figure 5. Influence of  $R_c$  on  $\phi(\zeta)$  concentration profile

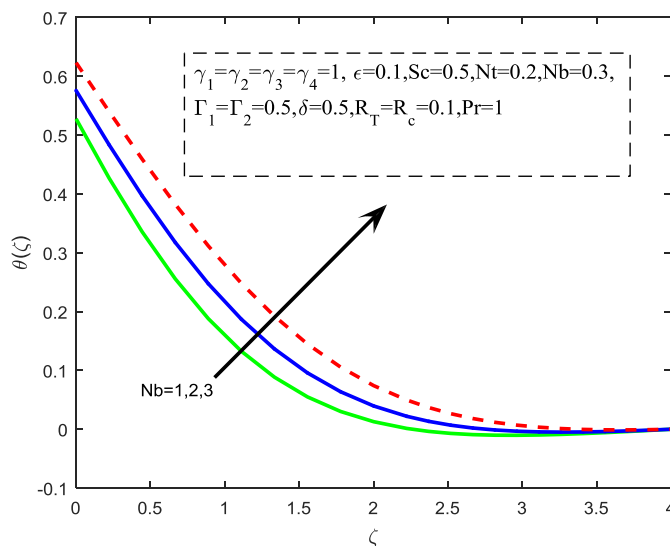


Figure 6. Influence of  $Nb$  on  $\theta(\zeta)$  temperature profile

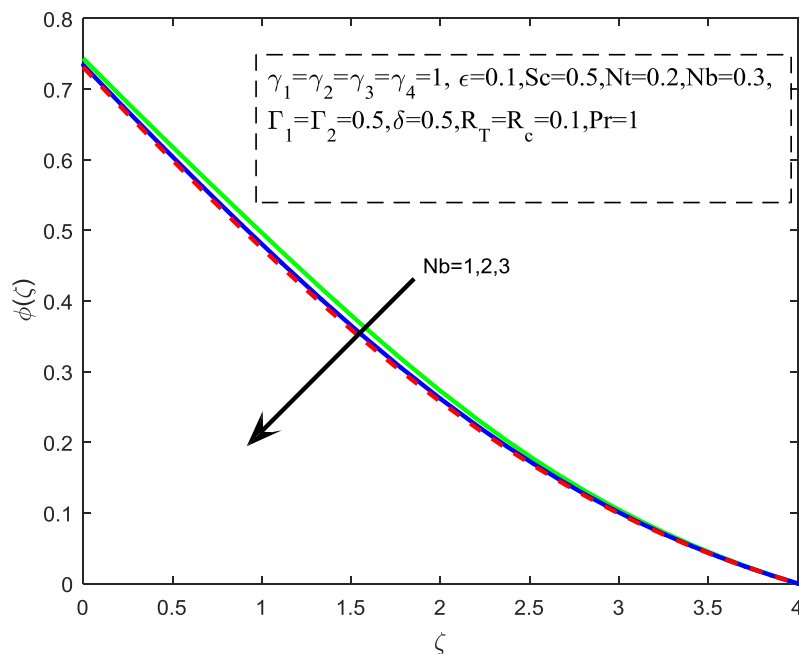


Figure 7. Influence of  $Nb$  on  $\phi(\zeta)$  concentration profile

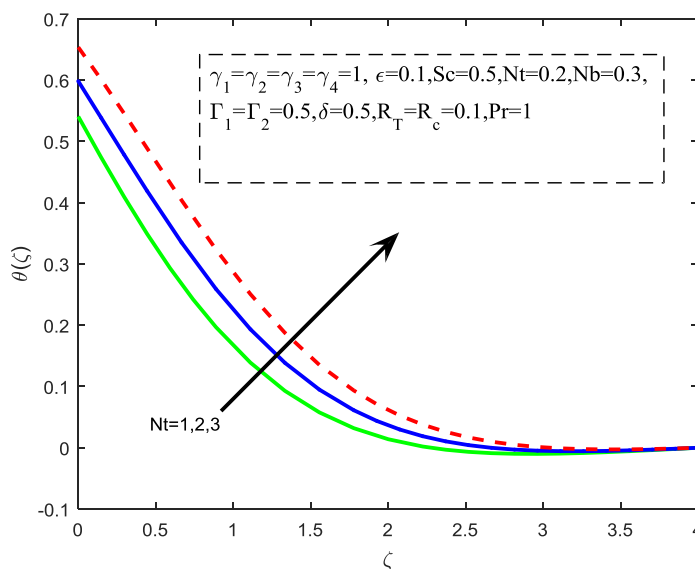


Figure 8. Influence of  $Nt$  on  $\theta(\zeta)$  temperature profile

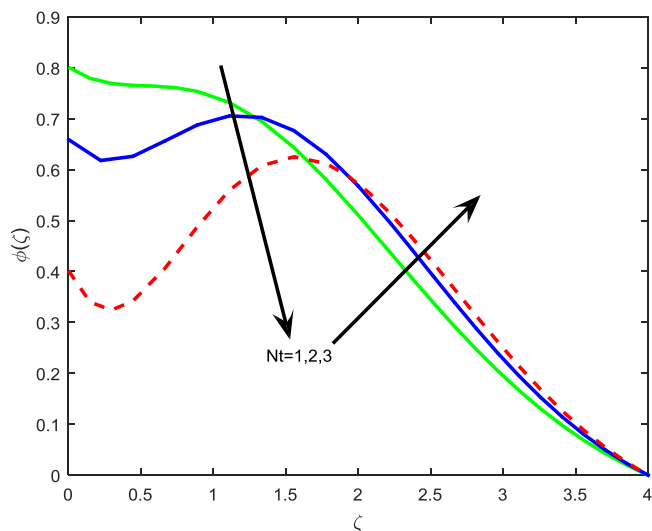


Figure 9. Influence of  $Nt$  on  $\phi(\zeta)$  concentration profile

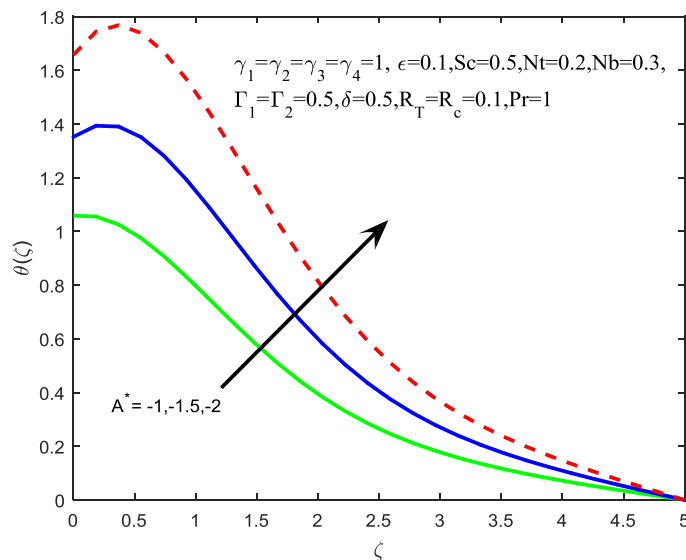


Figure 10. Influence of  $A^*$  on  $\theta(\zeta)$  temperature profile

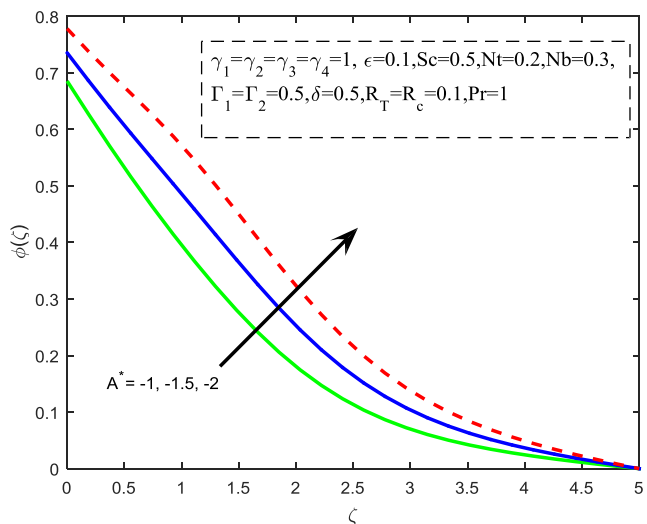


Figure 11. Influence of  $A^*$  on  $\phi(\zeta)$  concentration profile

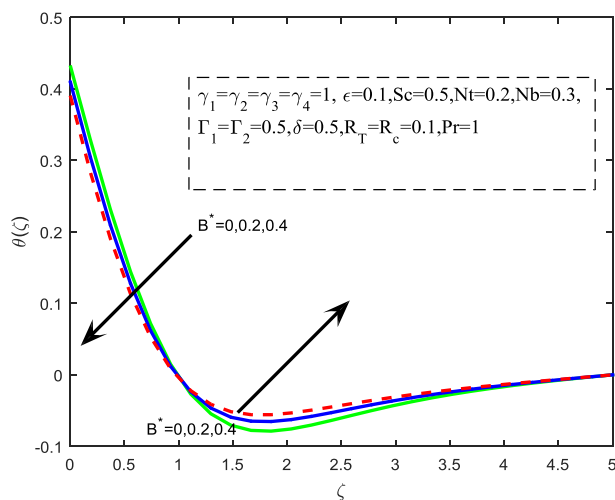


Figure 12. Influence of  $B^*$  on  $\theta(\zeta)$  temperature profile

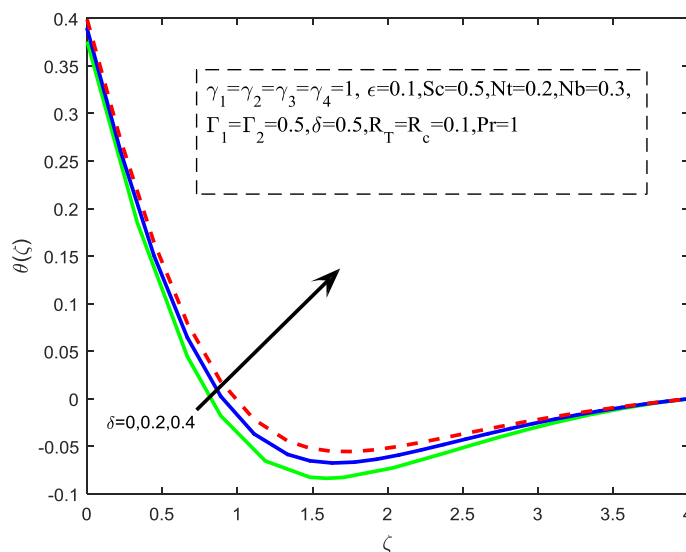


Figure 13. Influence of  $\delta$  on temperature profile

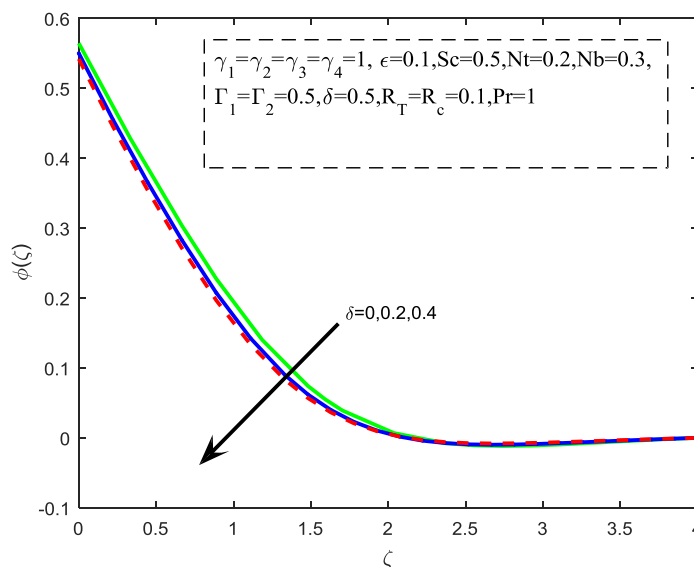


Figure 14. Influence of  $\delta$  on  $\phi(\zeta)$  concentration profile

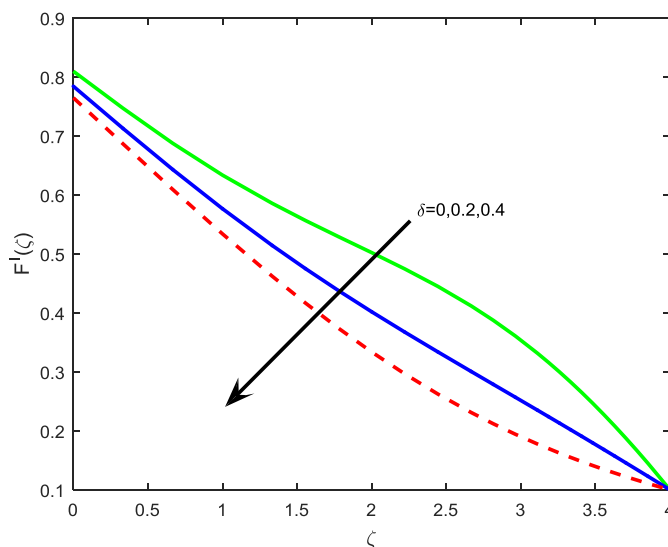


Figure 15. Influence of  $\delta$  on  $F'(\zeta)$  velocity profile

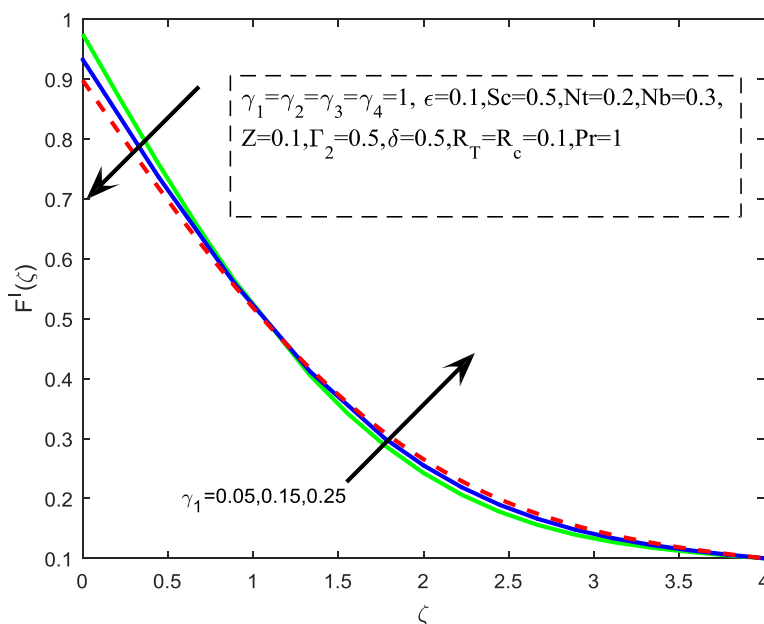


Figure 16. Influence of  $\Upsilon_1$  on velocity profile

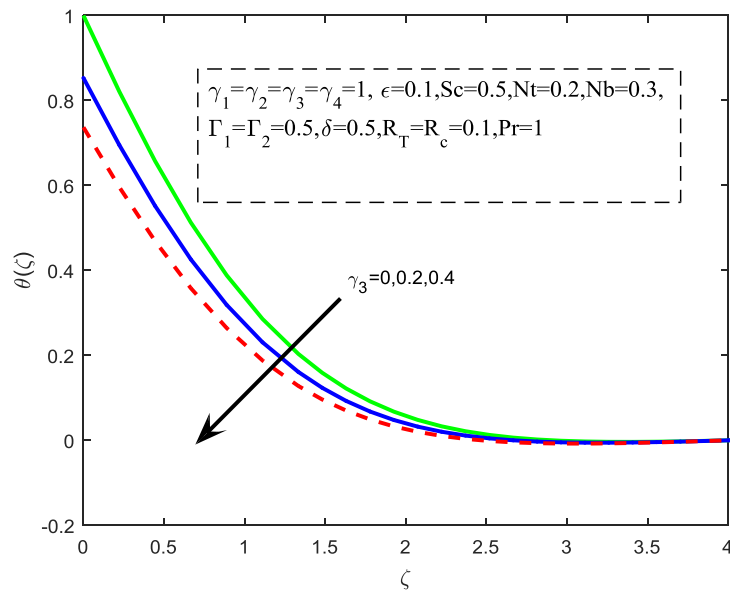


Figure 17. Influence of  $\Upsilon_3$  on  $\theta(\zeta)$  temperature profile

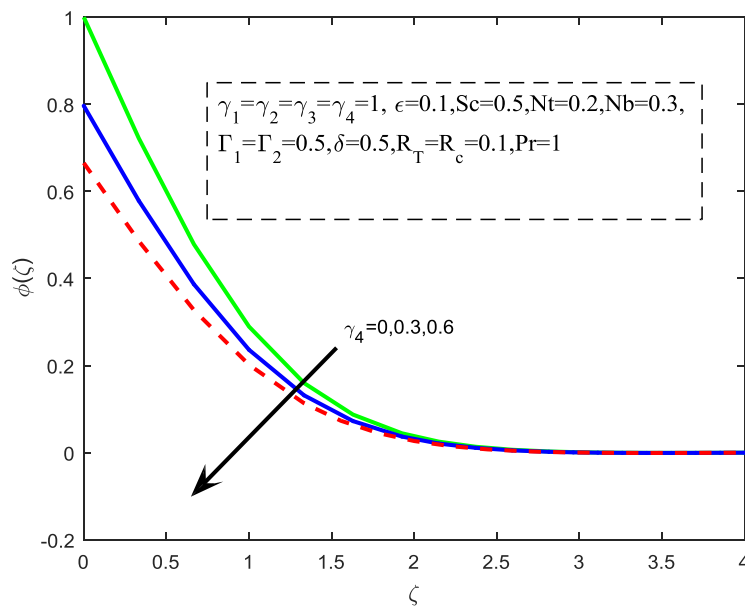


Figure 18. Influence of  $\Upsilon_4$  on  $\phi(\zeta)$  concentration profile





**Table I.** Comparison values of skin friction Coefficient  $\left(\frac{1}{2} C_{fx} Re_x^{1/2}\right)$  for different values of  $\Gamma_2$

when  $Y_1 = Y_2 = Y_3 = Y_4 = Z = Nt = Nb = A^* = B^* = \varepsilon = R_T = R_C = 0, Pr = Sc = 1$

$\Gamma_2$	Hakeem et al. [35 ]	Nayak et al. [28 ]	Present
0.3	1.19523	1.19523	1.19534
0.2	1.11803	1.11803	1.11804
0.1	1.05409	1.05409	1.05409
0.05	1.02598	1.02598	1.02598
0.01	1.00504	1.00504	1.005039
0	1.00000	1.00000	1.00000

**Table II.** Comparison values of local Nusselt number  $\left(\frac{1}{2} Nu_x Re_x^{1/2}\right)$  for different values of Pr

when  $Y_1 = Y_2 = Y_3 = Y_4 = Z = Nt = Nb = A^* = B^* = \Gamma_1 = \Gamma_2 = \varepsilon = R_T = R_C = 0, Sc = 1$

Pr	Present	Nayak et al. [28 ]	Awais et al. [34 ]
0.07	0.0665	0.0656	0.0663
0.2	0.1691	0.1691	0.1691
0.7	0.4544	0.4539	0.4534
2	0.9115	0.9114	0.9113
7	1.8954	1.8954	1.8954
20	3.3543	3.3539	3.3539

**Table III.** Comparison values of  $\left(\frac{1}{2} C_{fx} Re_x^{1/2}\right)$  and  $\left(\frac{1}{2} Nu_x Re_x^{1/2}\right)$  for different values of  $\varepsilon$  when

$Y_1 = Y_2 = Y_3 = Y_4 = Z = Nt = Nb = A^* = B^* = \Gamma_2 = R_T = R_C = 0, Pr = Sc = 1$

$\varepsilon$	$\left(\frac{1}{2} C_{fx} Re_x^{1/2}\right)$			$\left(\frac{1}{2} Nu_x Re_x^{1/2}\right)$		
	Present	Nayak et al. [28 ]	Nadeem et al. [33 ]	Present	Nayak et al. [28 ]	Nadeem et al. [33 ]
1	0.00000	0.00000	0.00000	0.7979	0.79788	0.79788
2	-2.0175	-2.01750	-2.01750	0.97875	0.97873	0.97873
3	-4.7293	-4.72928	-4.72928	1.13209	1.13209	1.13209
0.1	0.96938	0.96938	0.96938	0.6022	0.60216	0.60281
0.2	0.84943	0.84942	0.84942	0.6473	0.64728	0.64732
0.8	0.2994	0.29938	0.29938	0.7571	0.7571	0.75709



**Table IV.** Variation in values of  $\left(\frac{1}{2} C_{fx} Re_x^{1/2}\right)$ ,  $\left(\frac{1}{2} Nu_x Re_x^{-1/2}\right)$  and  $\left(\frac{1}{2} Sh_x Re_x^{-1/2}\right)$

Z	$R_T$	$R_C$	Nb	Nt	$A^*$	$B^*$	$\delta$	$\Upsilon_1$	$\Upsilon_3$	$\Upsilon_4$	$C_f Re_x^{1/2}$	$Nu_x Re_x^{-1/2}$	$Sh_x Re_x^{-1/2}$	Elapsed Time(sec onds)
0.1											-1.371024	0.321418	0.185062	0.666631
0.2											-1.295038	0.333470	0.181310	
0.3											-1.217145	0.344500	0.177636	
	1										-1.615951	0.515946	0.238104	0.693472
	2										-1.615951	0.531728	0.225539	
	3										-1.615951	0.544661	0.215339	
		1									-0.850619	0.507976	0.305900	0.737681
		1.5									-0.850619	0.509684	0.265342	
		2									-0.850619	0.510772	0.240153	
			1								-1.590979	0.472360	0.256519	0.624096
			2								-1.590979	0.424285	0.265884	
			3								-1.590979	0.376840	0.269054	
				1							-1.590979	0.459353	0.199036	0.696453
				2							-1.590979	0.401724	0.598307	
				3							-1.590979	0.346289	1.442431	
					-1						-0.851884	-0.058828	0.314556	0.884479
					-1.5						-0.851884	-0.352234	0.264695	
					-2						-0.851884	-0.657365	0.221907	
						0					-0.851884	0.567189	0.458482	0.868221
						0.2					-0.851884	0.589709	0.460556	
						0.4					-0.851884	0.609329	0.462570	
							0				-0.688593	0.624249	0.435595	0.758649
							0.2				-0.769789	0.611035	0.449909	
							0.4				-0.830111	0.601120	0.458037	
								0.05			-2.763047	0.526807	0.437537	0.728331
								0.15			-2.036706	0.516666	0.445517	
								0.25			-1.603918	0.510071	0.448880	
									0		-0.854660	0.831541	0.438390	0.678102
									0.2		-0.854660	0.735370	0.441395	
									0.4		-0.854660	0.657950	0.444218	
										0	-0.854660	0.479975	0.864147	0.777200
										0.3	-0.854660	0.487886	0.677982	
										0.6	-0.854660	0.492989	0.557805	



## 5. Concluding remarks

Influence of electromagnetic fields on stagnation point flow of the Walter's B nanofluid encompassing Brownian motion and the thermophoresis, Cattaneo-Christov thermal as well as solutal diffusion, non uniform heat source-sink and the multiple slip is described numerically. The foremost results of this study are:

- Walter's B nanofluid flow parallel to the electromagnetic sheet is assisted through Lorentz force.
- Enhancement in the  $F'(\zeta)$  is witnessed for larger values of  $Z$  and  $\Upsilon_1$  this signifies that fluid velocity surpasses from the free stream velocity.
- Electromagnetic sheet can be used for better cooling since improvement in  $Z$  declines  $\theta(\zeta)$ .
- $R_T$  decreases  $\theta(\zeta)$  and Cattaneo-Christov thermal diffusion can be used for cooling purpose.
- Rising values of  $R_C$  and  $Nt$  improves solutal boundary layer.
- $\theta(\zeta)$  increases via larger parameter values of  $Nb, Nt, \delta$
- Improvement in  $B^*$  shows mixed performance on temperature profile.
- Improvement in  $Z, R_T, R_C, A^*, B^*$  and  $\Upsilon_4$  improves heat transfer rate.
- Augmentation in solutal, velocity, thermal slip and parameters shrink the hydrodynamic, thermal and solutal boundary layer.
- Mass transfer is improved with elevating values of  $Nb, Nt, A^*, B^*, \delta, \Upsilon_1, \Upsilon_3$
- The average elapsed time required for computing the result is approximately 0.7 seconds.

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